

See discussions, stats, and author profiles for this publication at: <https://www.researchgate.net/publication/269279058>

# Control structure for Induction Motor Using Causal Informational Graph

Article · November 2014

---

CITATIONS  
0

READS  
119

1 author:



**Toufouti Riad**

Université Mohamed Chérif Messaadia de Souk-Ahras

35 PUBLICATIONS 348 CITATIONS

SEE PROFILE

# Control structure for Induction Motor Using Causal Informational Graph

S. Hassainia  
Department of Electrical  
Engineering,  
Univ.SoukAhras, Algeria  
sa\_hassainia@yahoo.fr

R.Toufouti Department  
of Electrical  
Engineering,  
Univ.SoukAhras, Algeria  
toufoutidz@yahoo.fr

S.Meziane  
Department of Electrical  
Engineering,  
Univ.SoukAhras, Algeria  
meziane\_elc@yahoo.fr

**Abstract**—In this paper, we'd like to present a tool for modeling and representing systems that allows a subsequent structuring of the control of these systems. This tool, which is the causal informational graph (CIG), allows to highlight the different relationships between energy variables in a system. Supplemented by another tool that is the macroscopic energy representation (MER), which insists on the principle of action and reaction between the different elements of the system. These tools enable a dual interest, first developing the model for the system structure and the control of this one. Simulation results show that the proposed modeling and control strategy can provide adequate control of the induction motor.

**Keywords**:-Causal Informational Graph(CIG), Inverse model of control , Induction machine, Field oriented control, macroscopic energy representation.

## 1. INTRODUCTION :

Growing economic challenges require more effective and efficient systems. The electro-mechanical conversion is thus ensured by electrical systems increasingly complex: Heavy chain drive kinematics, multi-computer systems, multi-convertors systems .. Control of such systems is a challenging task because it must respond to the management of energy transformation that occurs through several interacting elements.

Various tools have been developed to have a representation of ordered action of energetic variables in a system; they aim to support the implementation of system control under study. Amongst these tools, the causal informational graph (CIG) [1] is a graphical representation that allows a synthetic description of the relationships between the variables of a process according to the notion of cause and effect, then the structure of control can be deduced by reversing the graph.

In this paper the principles of CIG which will subsequently applied to determine a control algorithm for induction machine . The control is addressed in a modular approach.

## 2. CAUSAL INFORMATIONAL GRAPH CIG:

The Causal Ordering Graph (COG) is a graphical representation of mathematical equations, which can be used to model a system. The COG consists of a graphical language for describing dynamic

systems in a physical manner thanks to the use of the natural causality principle[9].

Processors are separate elements attached to an object or a set of localized objects within the studied process, it underpins a transformation relationship between one or more influencing magnitudes and an influenced magnitude; this relationship is induced by the principle of natural causality governing the energy operation of any object or group of objects. These transformational relations are of two types[1-9]:

2.1. *A rigid relationship*: bijective and reversible, independent of time, the input affects directly the output. causality is external.

2.2. *A causal relationship*: is characterized by a well defined input and output, cause and effect interchangeable, and the relationship depends on time (a variation of the input implies an evolution of the output with a transient and steady state). Causality is internal.

Fig.1 gives symbolism to differentiate the two types of processors.

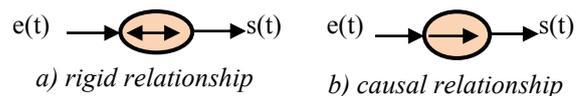


Fig.1: CIG representation of a processor

Natural causality for physical systems is integral causality: energy is a continuous function of time. Every physical entity may be represented by one or more connected processors.

## 3. MODEL CONTROL:

The ideal process control consists in the inversion of i main causality chain in order to define the control input depending on the desired output. Two types of inversion are defined: Rigid relationships are directly inverted show Fig2.a;

The causal relationships are reversed through an enslavement Fig.2b as their inputs and outputs are not interchangeable. [3]

An enslavement relationship allows indirectly reversing the non reversible relationship, but requiring an additional input, which is the actual output in order to minimize the gap and ensure the further reference

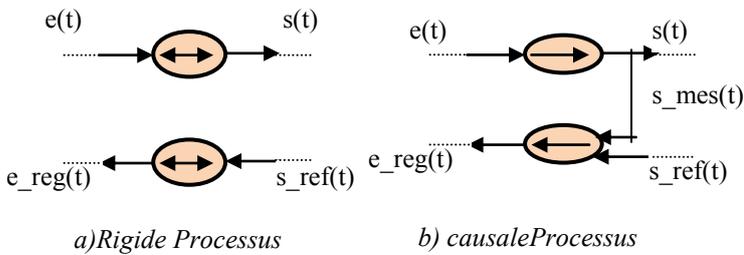


Fig.2 : Inversion des relations d'un GIC

#### 4. ENERGETIC MACROSCOPIC REPRESENTATION

The energetic macroscopic representation is a condensed CIG whose graph is organized and simplified to make proof of the exchange variables of elements of an energetic conversion.

A conversion of an electromagnetic chain relates an electric source ES to a mechanic source MC with:

- An electrical convertor EC which adapts electrical power between the source and the machine
- An electrical machine EM which secures an electromagnetic conversion
- A mechanic convertor MC which adapts the mechanic energy between the machine and the mechanic source.

Each of the conversion elements can dispose of a regulating vector . This representation makes proof the relationship of action and reaction between the different elements of the conversion chain, fig.3

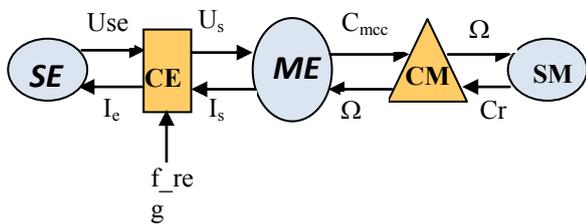
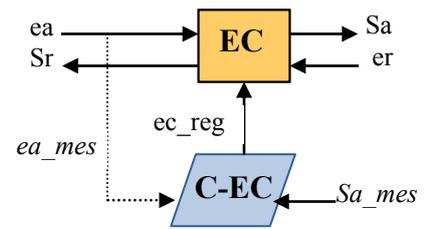
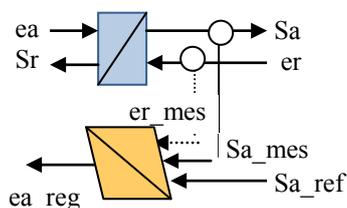


Fig.3 :The chain of electromagnetic conversion

In such chain, we can find that the accumulation elements are the elements that provide connection, the sources and the elements of conversion, the case of the windings of an electrical machine.

##### 4.1 Control Structure Deducd From aMER :

The CIG shows that the control of a process consists in the inversion of its model : find the right cause to generate the right effect; this principle is applied to the EMR in order to deduce the control structure of an electromagnetic conversion chain.



##### 4.2. Application :

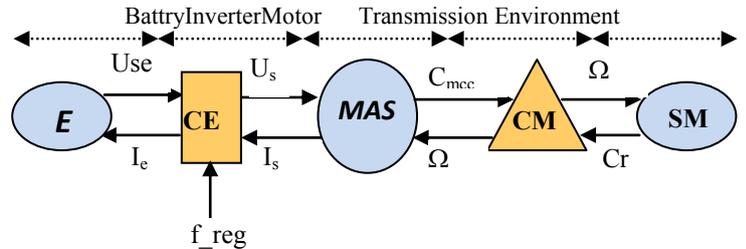


Fig.5 :EMR of a conversion chain

a) Sources definition: The electrical source imposes a continuous voltage  $U_{SE}$ , the mechanic source is assimilated to the load that the machine tows which imposes a resistant torque; we just need a constant resisting torque.

b) Representation of a static convertor : The static convertor is a three phase inverter characterized by its modulation function  $m_{ce}$  with

$$U_{ce} = \begin{bmatrix} |Va| \\ |Vb| \\ |Vc| \end{bmatrix} = m_{ce} \cdot U_{se}$$

$$\text{Where } m_{ce} = \frac{1}{3} \begin{bmatrix} 2 & -1 & -1 \\ -1 & 2 & -1 \\ -1 & -1 & 2 \end{bmatrix} \begin{bmatrix} f_{11} \\ f_{21} \\ f_{31} \end{bmatrix}$$

$f_{11}, f_{21}, f_{31}$ , constitutes the connection functions of the static switchers of the inverter

c) Representation of induction motor: The induction machine is considered classical, it is constituted of a stator, a rotor cage; the air gap is constant ; modeling is based on classical assumptions: unsaturated magnetic circuit, constant permeance, notch effects neglected. The equations of the induction machine defined in the arbitrary Park referential: The voltage equations is :

$$\begin{cases} V_{ds} = R_s i_{ds} + \frac{d\Phi_{ds}}{dt} - \omega_s \cdot \Phi_{qs} \\ V_{qs} = R_s i_{qs} + \frac{d\Phi_{qs}}{dt} + \omega_s \cdot \Phi_{ds} \\ V_{dr} = 0 = R_r i_{dr} + \frac{d\Phi_{dr}}{dt} - \omega_{rs} \cdot \Phi_{qr} \\ V_{qr} = 0 = R_r i_{qr} + \frac{d\Phi_{qr}}{dt} - \omega_{rs} \cdot \Phi_{ds} \end{cases} \quad (1)$$

Mechanical equations

$$J \frac{d\Omega}{dt} + f \cdot \Omega = C_{mec} - C_r \quad (2)$$

$$C_{em} = \frac{M}{L_r} \cdot (\Phi_{dr} \cdot i_{qs} - \Phi_{qr} \cdot i_{ds}) \quad (3)$$

Flux equations

$$\begin{cases} \Phi_{ds} = L_s i_{ds} + M i_{dr} \\ \Phi_{dr} = L_r i_{dr} + M i_{ds} \\ \Phi_{qs} = L_s i_{qs} + M i_{qr} \\ \Phi_{qr} = L_r i_{qr} + M i_{qs} \end{cases} \quad (4)$$

Autopilotage equations

$$\omega_s = \omega_r + p\Omega \quad (4)$$

The calculations carried out and related to the modeling of induction machine in the Park referential. linked to the turning field, considering state variables, statoric current and the rotoric flux lead to the following expressions:

$$\begin{cases} V_{ds} = R_s i_{ds} + \sigma L_s \frac{di_{ds}}{dt} + e_{ds} \\ V_{qs} = R_s i_{qs} + \sigma L_s \frac{di_{qs}}{dt} + e_{qs} \\ V_{dr} = 0 = R_r i_{dr} + \frac{d\Phi_{dr}}{dt} + e_{dr} \\ V_{qr} = 0 = R_r i_{qr} + \frac{d\Phi_{qr}}{dt} + e_{qr} \end{cases} \quad (5)$$

The  $e_{ds}$  and  $e_{qs}$  terms result from electromechanical and electromagnetic coupling between the windings similar to electromotive forces developed by a DC machine defined as follows:

$$\begin{cases} e_{ds} = -\frac{M \cdot R_r}{L_r} \Phi_{dr} - \sigma L_s \omega_s i_{qs} - \frac{M \cdot p}{L_r} \Omega \Phi_{qr} \\ e_{qs} = p \cdot \Omega \cdot \frac{M}{L_r} \Phi_{dr} + \sigma L_s \omega_s i_{ds} - \frac{M R_r^2}{L_r^2} \Phi_{qr} \\ e_{dr} = -(\omega_s - p \cdot \Omega) \Phi_{qr} + \frac{M}{L_r} R_r i_{ds} \\ e_{qr} = (\omega_s - p \cdot \Omega) \Phi_{dr} - \frac{M}{L_r} R_r i_{qs} \end{cases} \quad (6)$$

Thus the induction machine model is illustrated by the CIG of figure .6.

#### 4.3. Strategy of Control :

To control the induction machine, it is necessary to decouple the flux control and the current generating the torque. To this end, we call on a control called vector control which directs the flux on the axis of the Park referential by :  $\Phi_{dr} = \Phi_r$  et  $\Phi_{qr} = 0$ .

By using the voltage equations of the rotor, we will come to:

$$\begin{cases} M \cdot i_{ds} = \Phi_{dr} + \frac{L_r}{R_r} \frac{d\Phi_{dr}}{dt} \\ \omega_r \cdot \Phi_{dr} = \frac{M R_r}{L_r} i_{qs} \end{cases} \quad (7)$$

And the torque is

$$C_{em} = p \cdot \frac{M}{L_r} \cdot \Phi_{dr} \cdot i_{qs} \quad (8)$$

From these equations, two magnitudes are to be controlled, the flux and its position.

The flux is controlled by the current  $i_{ds}$  hence  $V_{ds}$ , the torque is controlled by the current  $i_{qs}$  hence  $V_{qs}$

For an indirect control, we impose :  $\Phi_{dr} = \Phi_{ref} = cste$

In respect to the rules of inversion of the CIG, we get to the control of the CIG fig.7 with speed correctors and current correctors ; to choose the correctors, we can introduce the conventional corrector PI ou IP or smart correctors.

Figure .8 illustrates the EMR of the conversion chain with the control axis brought out through Matlab Simulink.

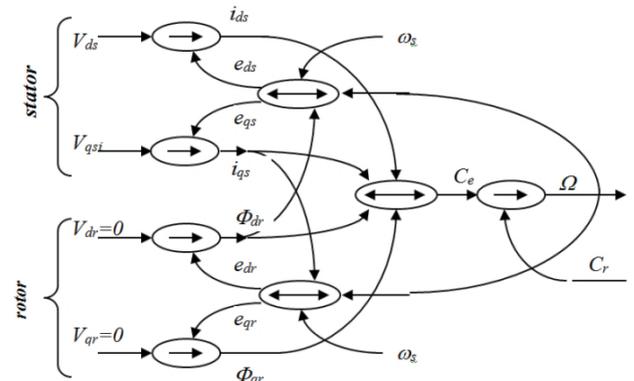


Fig.6 : GIC Representation of the induction motor

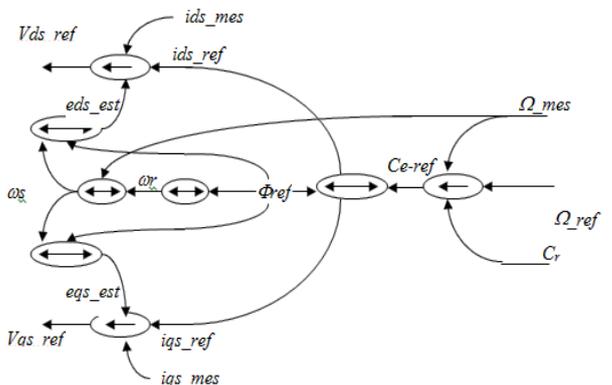


Fig.7 : Control scheme of the induction motor

#### 4.4. Simulation Results:

EMR and inversion-based control can be directly transposed to Simulink for Matlab (Fig. 8).

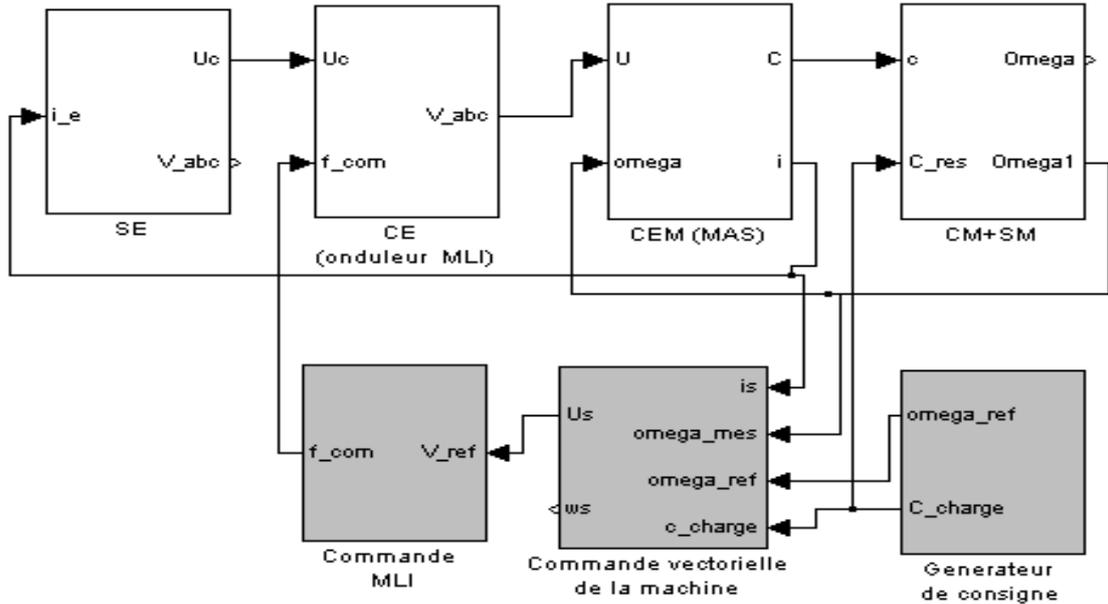


Fig.8. Structuring Control of an Induction Machine

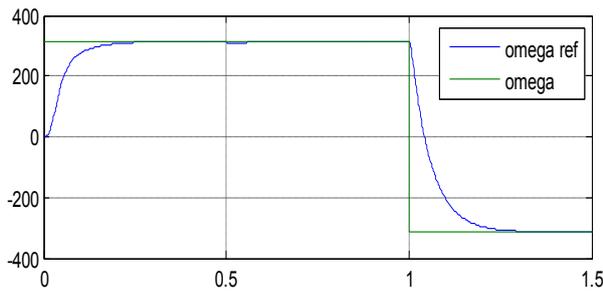


Fig.9a. Reference and rotor speed

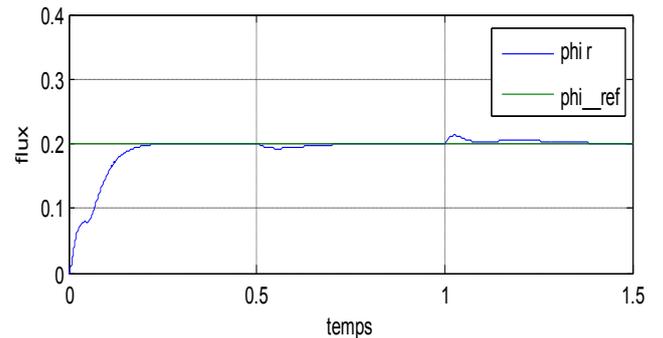


Fig.9d. Reference and rotor flux

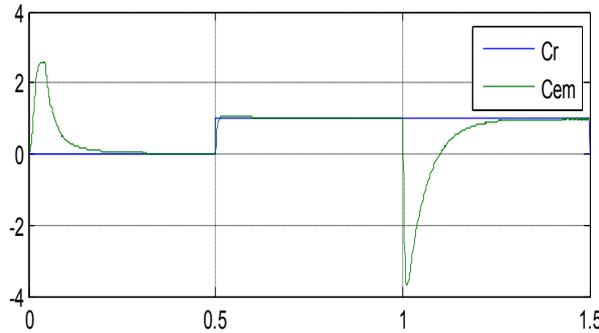


Fig.9b. Load and electromagnetic torques

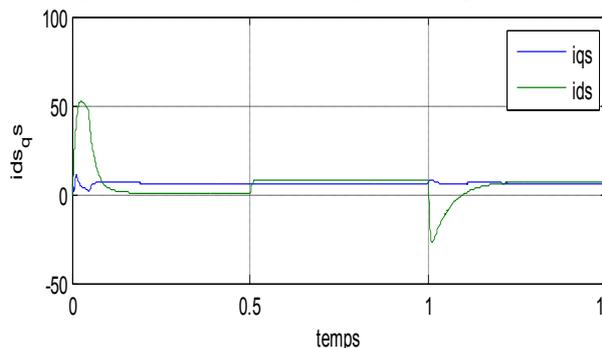


Fig.9c. Direct and quadrature stator current

The simulation results on the figures 9 (a-d) shows that a good tracking performance is achieved and the above results demonstrate that the proposed controller has strong robustness properties in the presence of load disturbance and parameter variations. Consequently, the use of the proposed cascade predictive nonlinear control scheme can solve the control problem of induction machines in the presence load torque variation.

From these results as it may be observed, the rotor speed tracks the desired speed in spite of system uncertainties. Moreover, the speed tracking is not affected by the load torque change (figures 9.a), since the electromagnetic and load torque quickly recovers the applied load torque value (figures9b).

As the figure show, the response of the flux is very good, because the real and estimate rotor flux rotor flux tracks the reference values adequately well (figures 7a and 7b). That figure shows the satisfying induction motor working, the rotor flux is maintained in independently of the electromagnetic torque.

## 5. CONCLUSION:

In this paper, we have presented a control structuring method of an electromagnetic conversion chain. The choice of the electromagnetic conversion chain concerning a chain with an induction machine in order to make proof of the usefulness of formalism CIG and its importance for structuring of electrical machine control laws and complex systems

This formalism (CIG) helps functional comprehension and description of the induction machine and allows the formulation of the machine control strategy by use of a simple logical reasoning that dwells in the step by step inversion of causalities. The inversion-based control deduced from these two graphical tools yields good performances of the tension regulation and the roll velocity tracking.

For future work the energetic macroscopic representation EMR can be used in different applications for experimental results: piezoactuators, tool machine, hybrid vehicle, polyphase machines, automatic subway, wind energy conversion systems.

## 6. RÉFÉRENCES :

- [1] S.Hassainia , H Abbassi , S.Kechida” “ Structuration de la commande pour une chaîne de conversion électromécanique à courant alternatif” 3<sup>rd</sup> International Conference : Science of Electronic, Technologies of Information and Telecommunication. Setit’2005, March 27-30 2005, Tunisia.
- [2] J. P Hautier , J. P Caron” Convertisseurs Statiques Méthodologie Causale de Modélisation et de Commande Ed Technique ”, Paris 1999.
- [3] P.J. Barre, J.P. Hautier, X. Guillaud and B.Lemaire-Semail, "Modelling and axis control of machine tool for high speed machining," in Proc. of the IFAC-IFIPIMACS Conference (CIS'97), Belfort, France, 1997.
- [4] A.Bouscayrol, X Guillaud, P.Delarue, J.P.Hautier ” Structure de Commande d'un Processus Mono Machine”, Séminaire SMM GDR SDSE Toulouse 18- 19 Novembre 1999.
- [5] A.Bouscayrol, T . Communal ” Approche Globale De La Commande Dynamique de Machine Electrique” : Revue 3ei N°.17, Juin 1999 Pp73 -79
- [6] S.Hassainia, H.Abbassi And S.Kechida, «The structuring of electro mechanic conversion drive chain» International Journal of soft Computing, Vol N°1 (3), pp:155-159, 2006.
- [7] Joseph Pierquin” Contribution à la Commande des Systèmes Multi Machine Multi - Convertisseurs Application à la Résolution De

Problèmes En Traction Electrique”.Thèse Présentée, De Doctorat de Université Lille Juillet 2002.

- [8] JiaZeng, Pierre-Jean Barre, Philippe Degort, “Modeling and Thrust Control of PMLSM Using Principle of Local Energy”, IEEE Conference Publications 2003, Sixth International Conference on Electrical Machines and Systems, Beijing, China, ICEMS 2003, 9-11 Nov, Vol N°:1 , pp: 26 - 30.
- [9] Ling Peng , Yongdong Li and Bruno Francois, “Modeling and Control of Doubly Fed Induction Generator Wind Turbines by Using Causal Ordering Graph during Voltage Dips” , IEEE Conference Publications 2008, International Conference on Electrical Machines and Systems, Wuhan, 17-20 Oct. 2008, Page(s): 2412 – 2417, ICEMS 2008.